

2. EVAPORATION (7 points) — *Solution by Jaan Kalda, grading schemes by Mattias Bjerklöv, Marko Tsengov, Eppu Leinonen.*

i) (2 points) Water is in a good approximation incompressible; hence, when the piston starts moving, the growing volume must be filled by gas which can be only the water vapours. Thus, the water starts boiling: these vapours must be in equilibrium with water, hence the vapour pressure must be equal to the pressure inside the piston. We can read from the graph that at T_0 , the vapour density is $\rho = 420 \text{ g m}^{-3}$; this corresponds to the pressure $p_1 = \rho RT / \mu = 70 \text{ kPa}$. With atmospheric pressure $p_0 = 100 \text{ kPa}$, the force

needed to pull the piston is $S(p_0 - p_1) = 300 \text{ N}$.

- Realize that the pressure inside the cylinder equals the saturated vapour pressure of water at temperature T_0 . **0.8 pts**
- Read the density ρ from the graph, in the range $[400, 440] \text{ g m}^{-3}$. **0.2 pts**
- Use the ideal gas law to find an expression for the pressure p_1 at temperature T_0 . **0.4 pts**
- Correct expression for the force: $S(p_0 - p_1)$. **0.4 pts**
- Correct numerical answer. **0.2 pts**

ii) (2 points) When the piston is pulled by displacement a , creating new volume $V_{\text{new}} = S \times a$, the water partially evaporates to fill this volume with vapour and the remaining liquid water cools from temperature T_0 to T_1 . The mass of vapour m_v needed to fill the new volume can be calculated using the vapour density $\rho_1 = 405 \text{ g m}^{-3}$ as $m_v = S a \rho_1$. For the heat balance, the energy needed for evaporation must come from the cooling of the remaining liquid water:

$$m_v L = (m - m_v) \cdot c \cdot (T_0 - T_1); \quad (1)$$

here we have neglected the dependence of L on temperature, and heat capacity of water vapours, because $\mu L \gg 4R(T_1 - T_0)$ (but we have not neglected the work done by piston, because L is actually the enthalpy of evaporation already includes $p\Delta V$). Similarly, since $L \gg c(T_1 - T_0)$, we can neglect m_v in the right-hand-side and express

$$m = \frac{m_v L}{c(T_0 - T_1)} = \frac{\rho_1 S a L}{c(T_0 - T_1)} = 650 \text{ g}. \quad (2)$$

- Read the vapour density ρ_1 from the graph ($\rho_1 \in [390, 420] \text{ g m}^{-3}$). **0.2 pts**
- Correct expression for mass of water vapour. **0.3 pts**
- Correct expression for the latent heat ($m_v L$). **0.3 pts**
- Correct expression for heat lost by water ($(m - m_v) \cdot c \cdot (T_0 - T_1)$). **0.3 pts**
- Expression for energy conservation. **0.4 pts**
- Correct expression for mass of water m . **0.3 pts**
- Correct numerical answer $m \in [630, 680] \text{ g}$ (with correct dimension). **0.2 pts**

iii) (3 points) At the thermal equilibrium, there is as much heat flux to the skin as there is heat loss due to evaporation. The former (per area) equals to $\kappa \frac{dT}{dx}$ and the latter (per area) — to $-LJm$ where m is the mass of one molecule, which we find to be $m = \mu/N_A$ to get $J\mu L/N_A$. Note that the minus sign comes from the fact that the particles diffuse from higher density areas to lower density areas. Now from the ideal gas law $n = P/Tk_B = PN_A/TR$ to get $J = -D \frac{d}{dx} \frac{rp}{Tk_B} = -D \frac{d}{dx} \frac{PN_A}{RT}$. Now the pressure of the water vapour is related to r through $P = rp$, where p denotes the saturation pressure of vapour. So,

$$\kappa \frac{dT}{dx} = -\frac{DL\mu}{R} \frac{d}{dx} \frac{rp}{T},$$

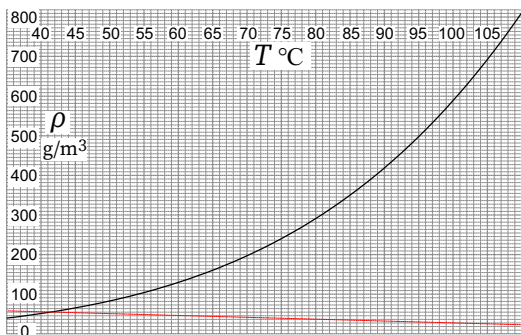
where $p = p(T)$ denotes the water vapour saturation pressure at the local air temperature; hence by integrating over x we obtain

$$\kappa(T - T_s) = \frac{DL\mu}{R} \left[\frac{p(T_s)}{T_s} - \frac{rp(T)}{T} \right],$$

where the index s denotes quantities evaluated at the skin surface. Also, we have used the fact that $r_s = 1$, because at the skin surface, the air is in direct contact with water (due to sweating, skin is wet), so that $pr_s = p(T_s)$. Substituting $\rho = \frac{p\mu}{RT}$ we obtain

$$\rho(T_s) = r\rho(T) + \frac{\kappa}{DL}(T - T_s).$$

Here we evaluate from the graph $r\rho(T) = 24.3 \text{ g m}^{-3}$ and $\frac{\kappa}{DL} = 0.51 \text{ g m}^{-3} \text{ K}^{-1}$. Now we can draw this straight line onto the graph provided to find the intersection point at $T_s = 41.5^\circ \text{C}$.



Grading: (preliminary)

NB! the $\rho = p\mu/RT$ substitution can be done earlier so the schemes below represent only the relevant observations which can be done with ρ already. Also equivalent forms will give points (i.e. if using k and N_a instead of R in the middle steps)

- heat going away from skin (up) = heat going to skin (down) at the equilibrium

0.4 pts

- Heat flux down $\kappa \frac{dT}{dx}$ **0.2 pts**

- Heat flux up magnitude $\frac{DL\mu}{R} \frac{d}{dx} \frac{P}{T}$ (partial points available for the equivalents to the steps below) **0.5 pts**

- Magnitude of heat flux up is LJm **0.3 pts**

- $m = \mu/N_A$ **0.1 pts**

- $n = P/Tk_B$ **0.1 pts**

- Deducing that the direction of the heat flow is opposite to $\frac{dn}{dx}$ (explicitly mentioned or with the existence of the minus sign in the equations) **0.1 pts**

- $P = rp$ **0.1 pts**

- $\kappa(T - T_s) = \frac{DL\mu}{R} \left[\frac{p(T_s)}{T_s} - \frac{rp(T)}{T} \right]$ (i.e. integrating correctly) **0.4 pts**

- Or doing a change from $d \rightarrow \Delta$ in the derivatives has to be motivated properly (i.e. for heat conductivity no need for any explicit explanation but for Fick's law one must state that J is constant (due to the amount of particles is conserved)).

- $\rho = p\mu/RT$ **0.1 pts**

- Reading ρ correctly ($\rho_1 \in [800,815]\text{gm}^{-3}$)

0.2p pts

- Graphical method **0.8 pts**

- Noticing that $\rho(T_s) = r\rho(T) + \frac{\kappa}{DL}(T - T_s)$ defines a straight line in (T, ρ) **0.8 pts**

- Any other valid numerical method that is explained is accepted

- Correct final result $T \in [36,47]^\circ\text{C}$ **0.2 pts**

If working with ρ earlier on one can show that that the heat flux up magnitude is

Solution 2 by Eppu Leinonen: One can also work directly with ρ through the fact that $n = N/V = MN_A/\mu V = \rho N_A/\mu$. Then the heat flux magnitude will directly become $LJm = LmD \frac{dn}{dx} = LmD \frac{N_A}{\mu} \frac{d\rho}{dx} = LD \frac{d\rho_v}{dx}$, where ρ_v is the density of the water vapour. Then with correct signs we get

$$\kappa \frac{dT}{dx} = -LD \frac{d\rho_v}{dx}$$

from which by integrating and using $\rho_v = r\rho$ we get

$$\rho(T_s) = r\rho(T) + \frac{\kappa}{DL}(T - T_s)$$

and the solution proceeds the same way as in solution 1.

The following grading scheme is given to provide exact correspondences to the scheme of solution 1. **Grading:**

- heat going away from skin (up) = heat going to skin (down) at the equilibrium
0.4 pts
- Heat flux down $\kappa \frac{dT}{dx}$ **0.2 pts**
- Heat flux up magnitude $LD \frac{d\rho_v}{dx}$ (partial points available for the equivalents to the steps below) **0.6 pts**
 - Working with ρ directly **0.1 pts**
 - Magnitude of heat flux up is LJm **0.3 pts**
 - $n = \rho N_A / \mu$ **0.1 pts**
 - $\mu = m N_A$ **0.1 pts**
- Deducing that the direction of the heat flow is opposite to $\frac{dn}{dx}$ (explicitly mentioned or with the existence of the minus sign in the equations) **0.1 pts**
- $\rho_v = r\rho_v$ **0.1 pts**
- $\kappa(T - T_s) = LD(\rho(T_s) - r\rho(T))$ (i.e. integrating correctly) **0.4 pts**
 - Or doing a change from $d \rightarrow \Delta$ in the derivatives has to be motivated properly (i.e. for heat conductivity no need for any explicit explanation but for Fick's law one must state that J is constant (due to the amount of particles is conserved)).
- Reading ρ correctly ($\rho_1 \in [800, 815] \text{gm}^{-3}$) **0.2p pts**
- Graphical method **0.8 pts**
 - Noticing that $\rho(T_s) = r\rho(T) + \frac{\kappa}{DL}(T - T_s)$ defines a straight line in (T, ρ) **0.8 pts**
 - Any other valid numerical method that is explained is accepted
- Correct final result $T \in [36, 47]^\circ\text{C}$ **0.2 pts**